

a<sup>1</sup> FIG. 5 is a schematic view showing one example of one of hybrid lens structures through which laser beams of the forwardly deflecting optical system of the optical scanning device shown in FIG. 2 pass;

On page 9, delete 3<sup>rd</sup> full paragraph (lines 12-15), and replace this paragraph with the following in accordance with 37 C.F.R. §1.121. A marked up version showing changes is attached:

a<sup>2</sup> FIG. 6 is a schematic view for explaining one of hybrid lenses through which laser beams of the forwardly deflecting optical system of optical scanning device shown in FIG. 2 pass, respectively;

On page 9, delete 4<sup>th</sup> full paragraph (lines 16-19), and replace this paragraph with the following in accordance with 37 C.F.R. §1.121. A marked up version showing changes is attached:

a<sup>3</sup> FIG. 7 is a schematic view for explaining one of hybrid lenses through which laser beams of the forwardly deflecting optical system of the optical scanning device shown in FIG. 2 pass, respectively;

On page 21, Table 2 delete 3<sup>rd</sup> & 4<sup>th</sup> headings, and replace these headings with the following in accordance with 37 C.F.R. §1.121. A marked up version showing changes is attached:

a<sup>4</sup> Lens surface No. 3 (incidence plane of lens 30b) coefficient

a<sup>5</sup> Lens surface No. 4 (ejection plane of lens 30b) coefficient

On page 22, delete 2nd full paragraph (lines 6-16), and replace this paragraph with the following in accordance with 37 C.F.R. §1.121. A marked up version showing changes is attached:

a<sup>6</sup> If an imaging lens set 30 that has two image-forming lenses 30a and 30b are included in the post deflecting optical system 21 under a condition that intervals between the plurality of beams are maintained constantly in all the scanning regions, wave aberration can not be corrected with a conventional toric lens or symmetry rotation aspheric surface having symmetry axis of rotation, and the image surface beam

a<sup>6</sup> cont.  
diameter can not be stopped down to 100  $\mu\text{m}$  or smaller. This fact was found by simulation and therefore, the lens of the post deflecting optical system shown in tables 1 and 2 has the above-described shape.

On page 22, delete 3<sup>rd</sup> full paragraph (lines 17-25), and replace this paragraph with the following in accordance with 37 C.F.R. §1.121. A marked up version showing changes is attached:

a<sup>7</sup>  
Since lens surfaces (incident surface of 30a, incident surface of 30b, leaving surface of 30a and leaving surface of 30b) of each of the two image-forming (the imaging lens set 30) are formed into the shape having no symmetry axis of rotation, it is possible to stop down the image surface beam diameter to about 50  $\mu\text{m}$  while constantly maintaining the intervals between the plurality of beams in all the scanning regions.

On page 24, delete 3<sup>rd</sup> full paragraph (lines 23-26), and replace this paragraph with the following in accordance with 37 C.F.R. §1.121. A marked up version showing changes is attached:

a<sup>8</sup>  
Here, the forwardly deflecting optical system 7Y will be explained as a representative of laser beam 3Ya ejected from the first yellow laser 3Ya to the polygonal mirror unit 5, as shown in FIG. 4.

On page 25, delete 2nd full paragraph (lines 9-13), and replace this paragraph with the following in accordance with 37 C.F.R. §1.121. A marked up version showing changes is attached:

a<sup>9</sup>  
A half mirror 12Y is inserted in between the finite focal lens 9Ya and the hybrid lens 11Y at a predetermined angle with respect to an optical axis between the infinite focal lens 9Ya and the hybrid lens 11Y.

On page 25, delete 3<sup>rd</sup> full paragraph (lines 14-27), and replace this paragraph with the following in accordance with 37 C.F.R. §1.121. A marked up version showing changes is attached:

a<sup>10</sup>  
On a surface opposite from a surface which the laser beam Lya enters from the first yellow laser 3Ya on the half mirror 12Y, a laser beam Lyb from the second yellow

A'10  
cont.

laser 3Yb disposed such that a predetermined beam distance can be provided in the sub-scanning direction with respect to the laser beam Lya from the first yellow laser 3Ya enters at a predetermined beam distance in the sub-scanning direction with respect to the laser beam Lya from the first yellow laser 3Ya. A finite local lens 9Yb and an aperture 10Yb are disposed between the second yellow laser 3Yb and the half mirror 12Y for converging the laser beam Lyb from the second yellow laser 3Yb to a predetermined value.

On page 26, delete 2nd full paragraph (lines 7-11), and replace this paragraph with the following in accordance with 37 C.F.R. §1.121. A marked up version showing changes is attached:

A'11

As the finite focal lenses 9 (Y, M, C and B) a and 9 (Y, M, C and B) b, an aspherical glass lens or a single lens comprising an aspherical glass lens and UV cure plastic aspheric lens laminated on the aspherical glass lens can be utilized.

On page 26, delete 3<sup>rd</sup> full paragraph (lines 12-19), and replace this paragraph with the following in accordance with 37 C.F.R. §1.121. A marked up version showing changes is attached:

A'12

As shown in Fig. 4, the hybrid lens 11Y is formed with a PMMA lens 17Y and a glass cylinder lens 19Y. The hybrid lens 11Y has a structure in which the lens 17Y and the cylinder lens 19Y has an air layer between the leaving surface of the lens 17Y and the cylinder lens 19Y, and a portion of the lens through which light does not pass is provided with a portion in which both the lenses are in contact with each other, shown in Fig. 5.

On page 26, delete 4<sup>th</sup> full paragraph (lines 20-24), and replace this paragraph with the following in accordance with 37 C.F.R. §1.121. A marked up version showing changes is attached:

A'13

The post deflecting optical system 21 including the imaging lens set has the positive power in the sub-scanning direction, and if a temperature rises, index of refraction is reduced and the lens is expanded and thus, the power (symbol is + (plus)) is reduced.

Delete the paragraph spanning pages 27 and 28 (page 27, line 26 to page 28, line 11), and replace this paragraph with the following in accordance with 37 C.F.R. §1.121. A marked up version showing changes is attached:

A<sup>14</sup>  
However, if the air layer is inserted as shown in Fig. 5, a region which is in contact with the glass lens and has the glass shape and a region having the original plastic lens shape are generated in a region through which the light of plastic passes as shown in FIG. 5. If there is a slight deviation in shape of both the surfaces, the focus position is deviated between the region having the glass shape and the region of the plastic lens, which makes it difficult to obtain optical beam shape at one location. The first embodiment has a structure for solving the above problem, as shown in Fig. 6.

On page 28, delete 1st full paragraph (lines 12-15), and replace this paragraph with the following in accordance with 37 C.F.R. §1.121. A marked up version showing changes is attached:

A<sup>15</sup>  
As shown in FIG. 6, the plastic lens 17 is made of material such as PMMA (polymethyl methacrylate). The glass cylinder lens 19 is made of material such as SF6.

On page 28, delete 2nd full paragraph (lines 16-23), and replace this paragraph with the following in accordance with 37 C.F.R. §1.121. A marked up version showing changes is attached:

A<sup>16</sup>  
When the plastic lens 17 of the hybrid cylinder lens 11 has a surface of negative power in the sub-scanning direction, and the plastic lens 17 and the glass cylinder lens 19 are assembled, a space portion is formed while sandwiching one convex surface of the glass cylinder lens 19, and the plastic lens 17 has at least two of the projection portions 17a abutting in the convex surface.

On page 29, delete 2nd full paragraph (lines 13-23), and replace this paragraph with the following in accordance with 37 C.F.R. §1.121. A marked up version showing changes is attached:

A<sup>17</sup>  
FIG. 7 is for explaining another embodiment of the optical scanning device of the present invention. The hybrid cylinder lens 11 has a includes a one side convex glass cylinder having curvature of substantially the same absolute value as that of the resin lens having negative power surface and having positive power in the sub-scanning